AeroTex Predictions for the 1st AIAA Ice Prediction Workshop

Simulations using OpenFOAM, TAC3D+ and ITA

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SIMULATION APPROACH



Simulation Approach

- OpenFOAM CFD
 - Incompressible
 - SIMPLE algorithm (Semi-Implicit Method for Pressure Linked Equations)
 - Spalart-Allmaras wall function
 - One equation model based on a modified turbulence viscosity
 - Widely used within the aerospace industry
 - Includes mesher: snappyHexMesh
 - All cases were re-meshed from the provided CAD, as there is no simple way to convert meshes to OpenFOAM format, and meshes generated in other software often causes issues

Simulation Approach (cont.)

TAC3D+ impingement

- AeroTex proprietary solver
- Calls OpenFOAM to perform Lagrangian droplet tracking
 - 4th order Runge-Kutta scheme
- Additional proprietary routines to calculate the surface collection efficiency
- Includes automatic refinement to optimise number of trajectories launched

ITA

- AeroTex proprietary solver
- Modified Messinger heat balance approach to determine freezing fraction and ice growth rates
- Single shot prediction, based on clean surface ice growth rates



Simulation Approach (cont.)

- TAC2 / IHB
 - AeroTex proprietary
 - 2D simulation tools
 - Combined inviscid, potential flow solver with Messinger heat balance
 - Lagrangian droplet tracking (4th order Runge-Kutta)

- 2D simulations included for selected cases
 - All 2D simulations utilised a single shot to compare to 3D cases

Computational Machine

- Single machine
 - AMD Ryzen Threadripper 3970X, 32 core
 - 256GB DDR4 RAM, 2667MHz
- Meshing and aerodynamic solutions were computed using 32 cores
- Impingement solution was computed using 8 cores per droplet bin for most cases
 - Increased to 16 cores per droplet bin for largest mesh case

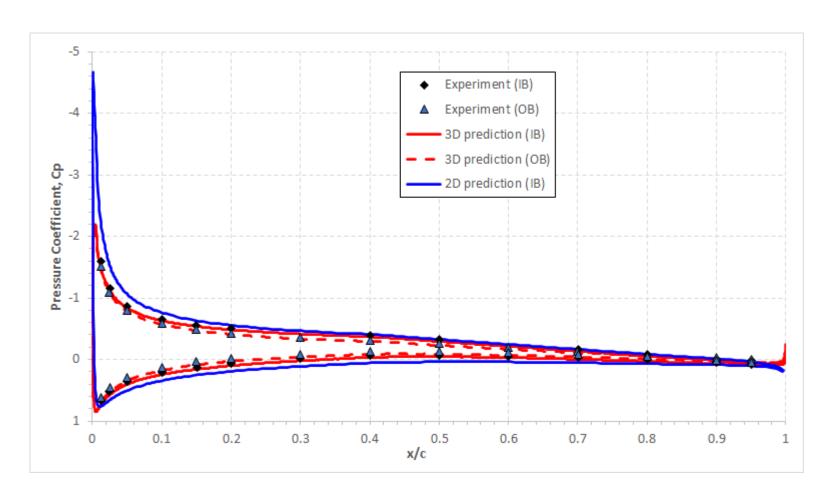
COLLECTION EFFICIENCY CASES

Case 111 and Case 112

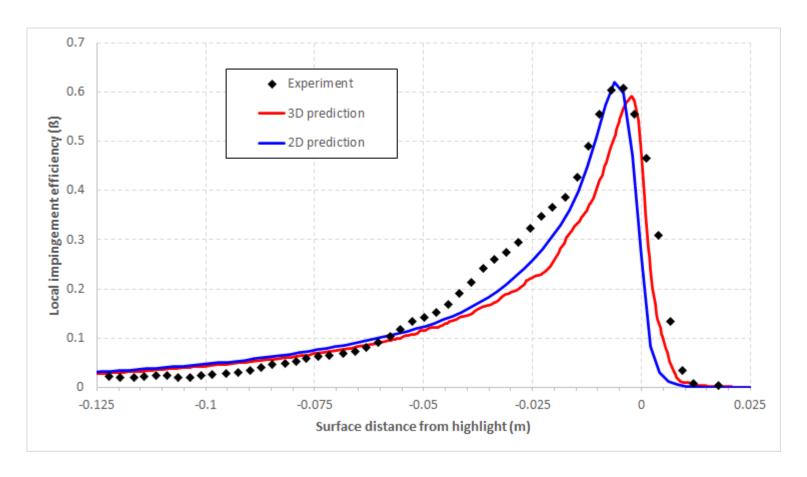
- NACA 64A008 H-Tail, $\alpha = 6^{\circ}$
 - Case 111 is MVD = 21 microns (27-bin)
 - Case 112 is MVD = 92 microns (27-bin)
- Modelled within IRT, including walls (3D)
- 9.01 million cells
- 92 micron case includes SLD corrections for splash and bounce
- Solver times:
 - Meshing = 645s (00:10:45)
 - Aerodynamics = 8390s (02:19:50)
 - Impingement = 3681s (01:01:21)



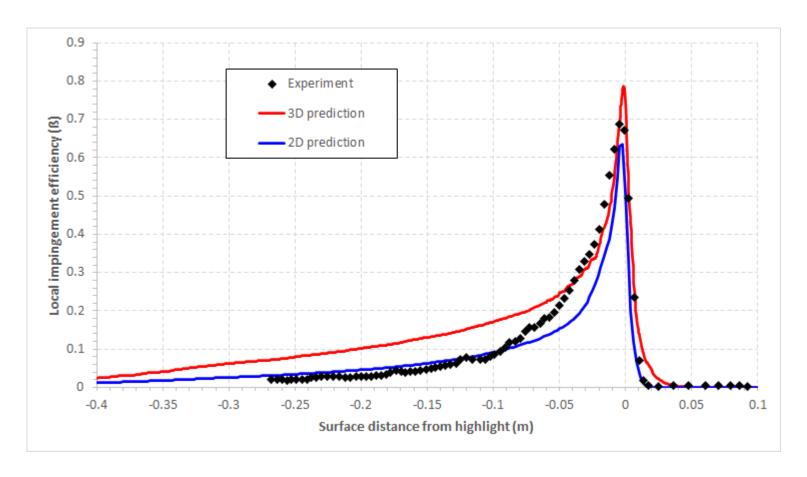
• Pressure coefficient



Local collection efficiency



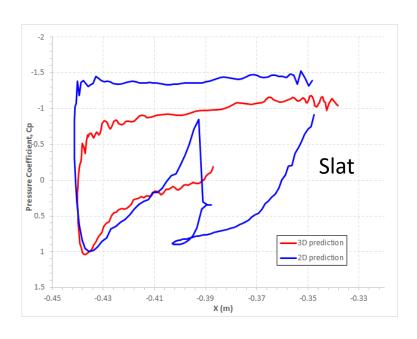
Local collection efficiency

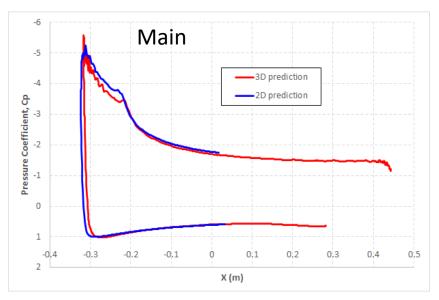


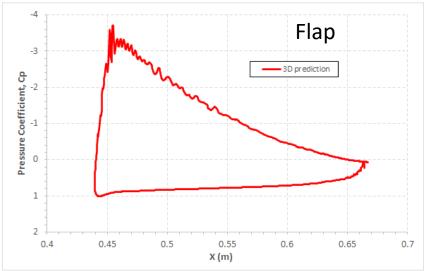
Case 121 and 122

- Three-element airfoil, $\alpha = 4^{\circ}$
 - Case 121 is MVD = 21 microns (27-bin)
 - Case 122 is MVD = 92 microns (27-bin)
- Modelled within IRT, including walls (3D)
- 34.32 million cells
- 92 micron case includes SLD corrections for splash and bounce
- Solver times:
 - Meshing = 5613s (01:30:33)
 - Aerodynamics = 24184s (06:43:04)
 - Impingement = 18938s (05:15:38)

• Pressure coefficient

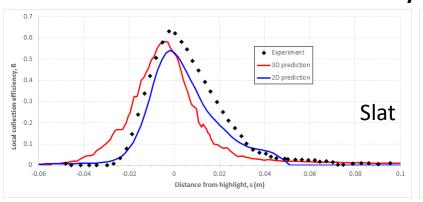


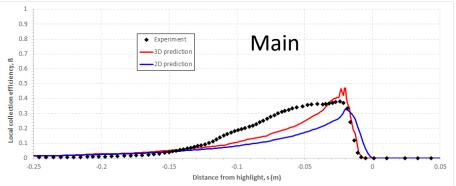


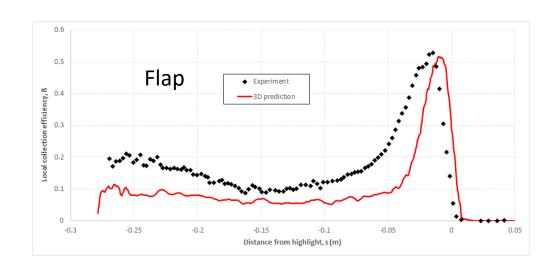




Local collection efficiency

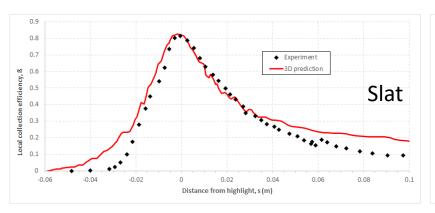


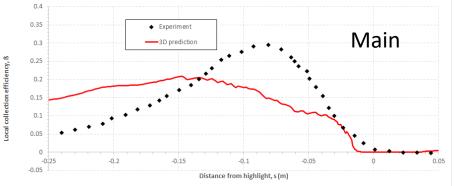


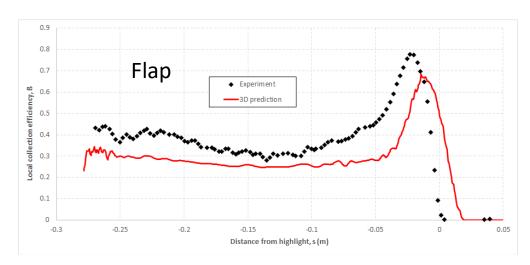




Local collection efficiency







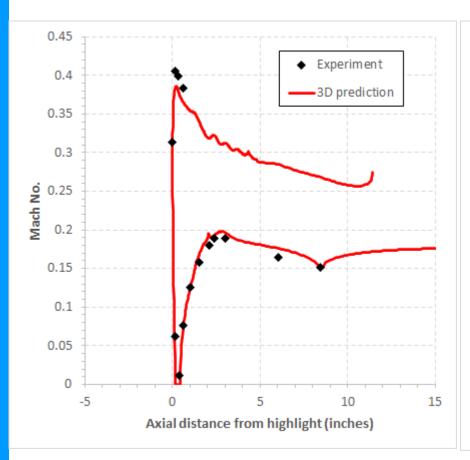


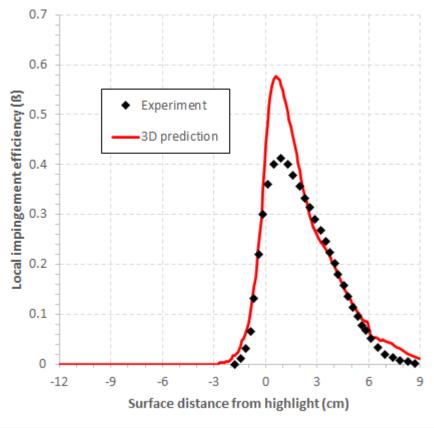
Case 131 and 132

- Axisymmetric inlet, $\alpha = 15^{\circ}$
 - Case 131 is lower mass flow (7.8kg/s)
 - Case 132 is higher mass flow (10.41kg/s)
- Both cases are MVD = 20 microns (7-bin)
- Modelled within IRT, including walls
- 6.57 million cells
- Solver times:
 - Meshing = 600s (00:10:00)
 - Aerodynamics = 6867s (01:54:27)
 - Impingement = 3376s (00:56:16)



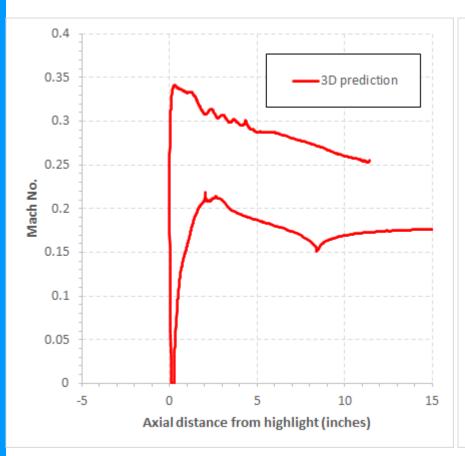
Theta 0 deg.

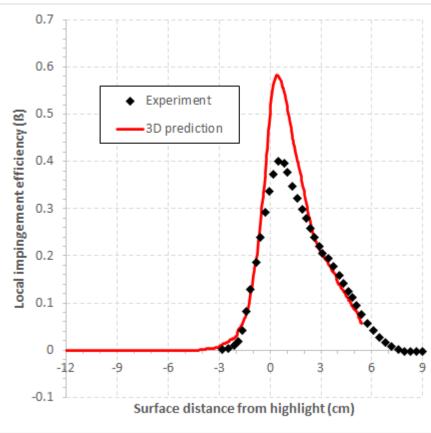






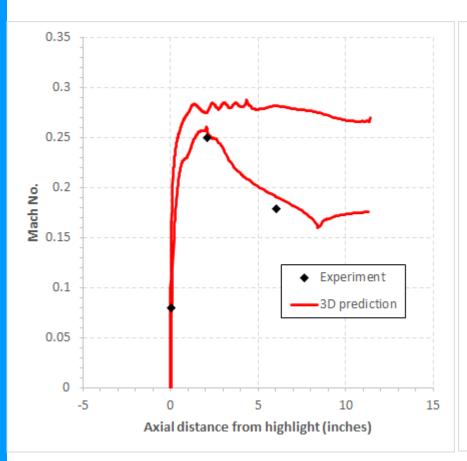
Theta 45 deg.

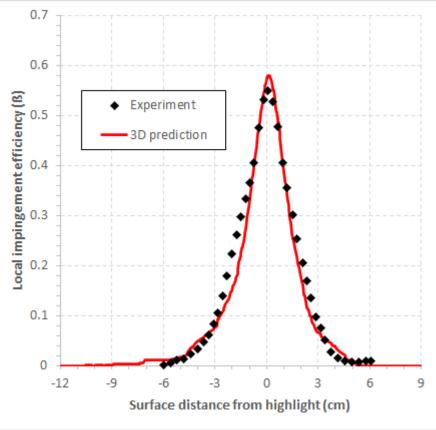




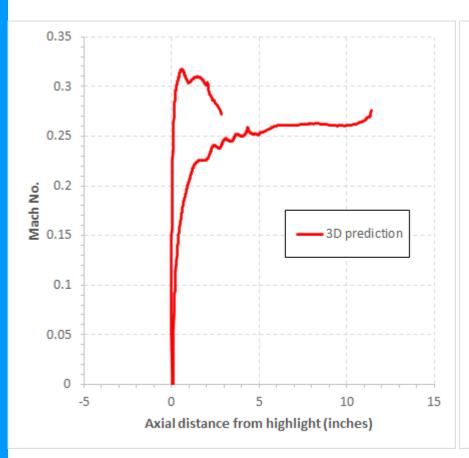


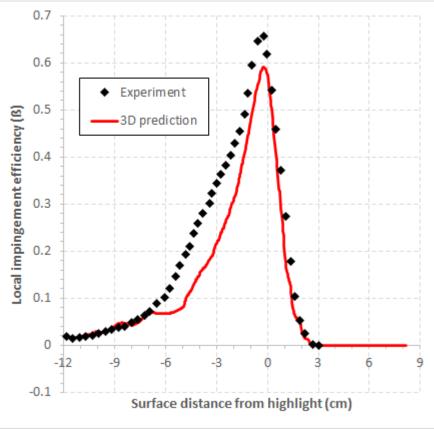
Theta 90 deg.



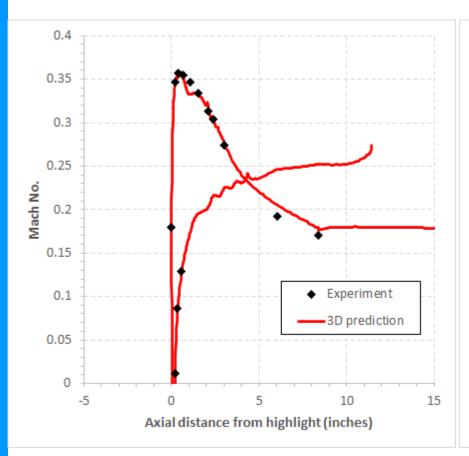


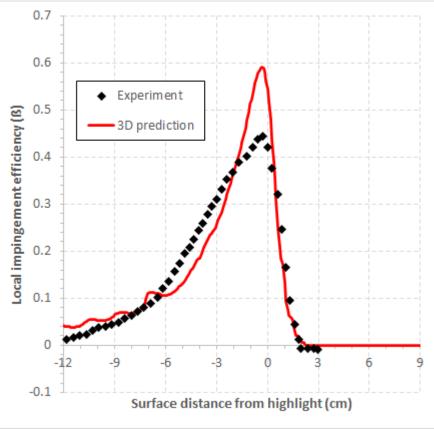
• Theta 135 deg.



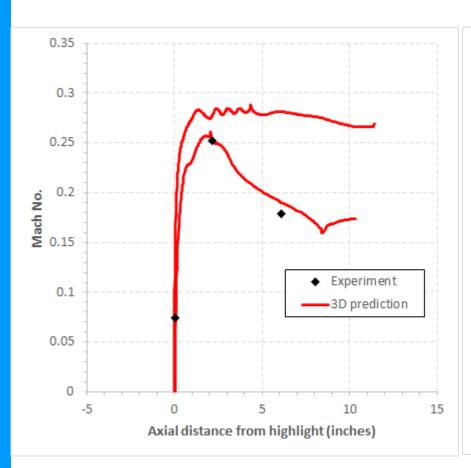


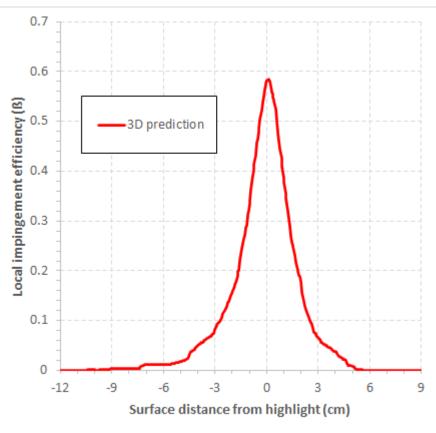
Theta 180 deg.



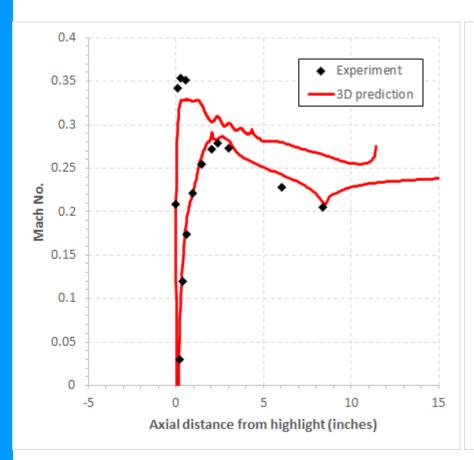


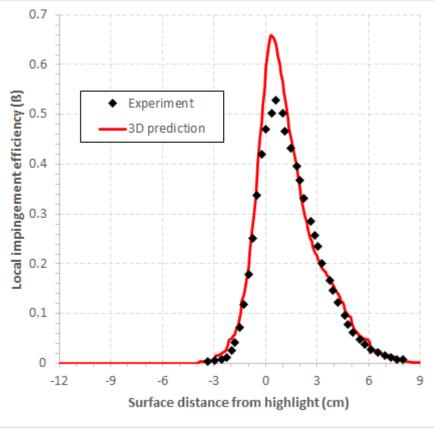
Theta 270 deg.





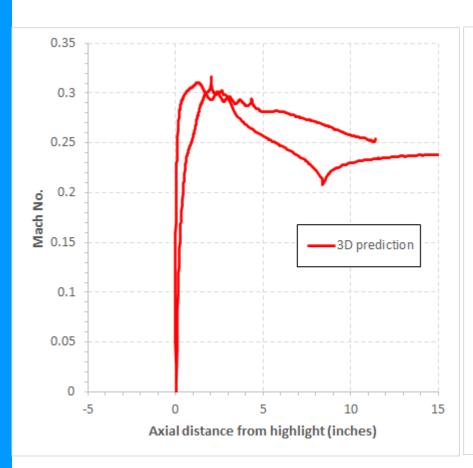
Theta 0 deg.

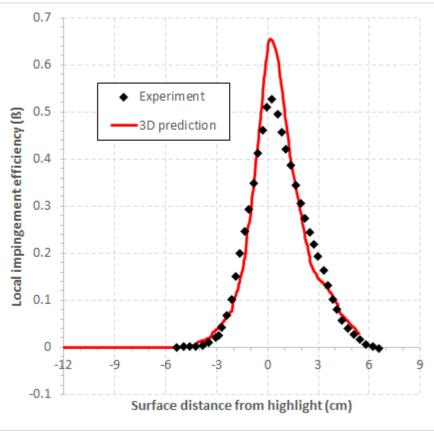




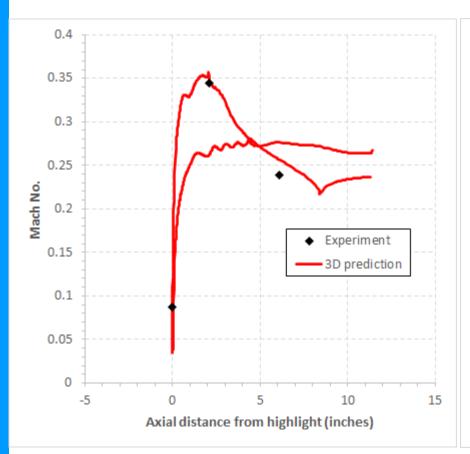


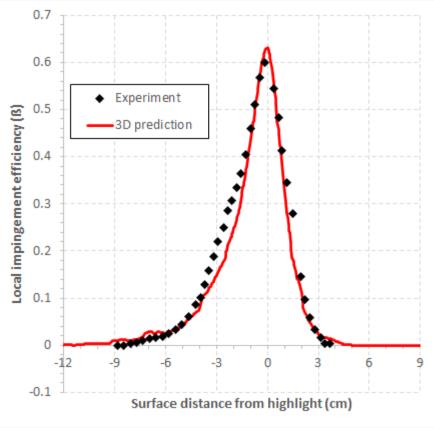
Theta 45 deg.





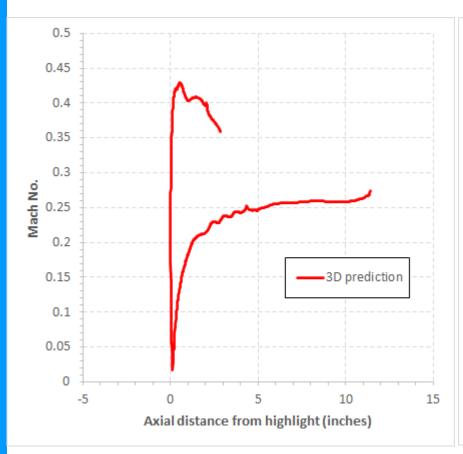
Theta 90 deg.

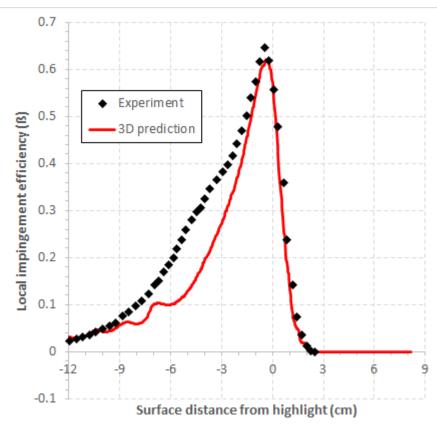




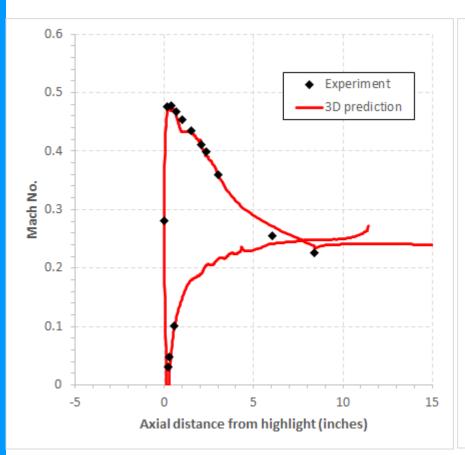


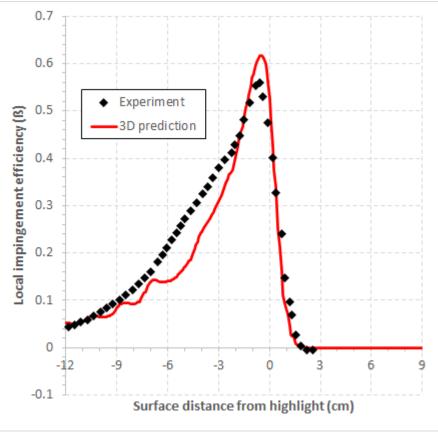
Theta 135 deg.





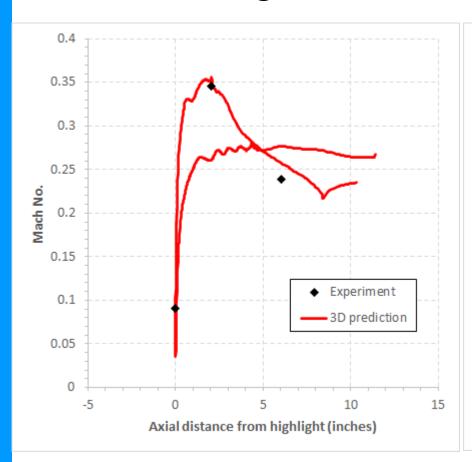
• Theta 180 deg.

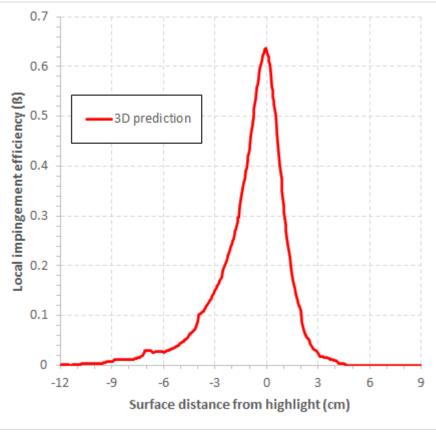






Theta 270 deg.





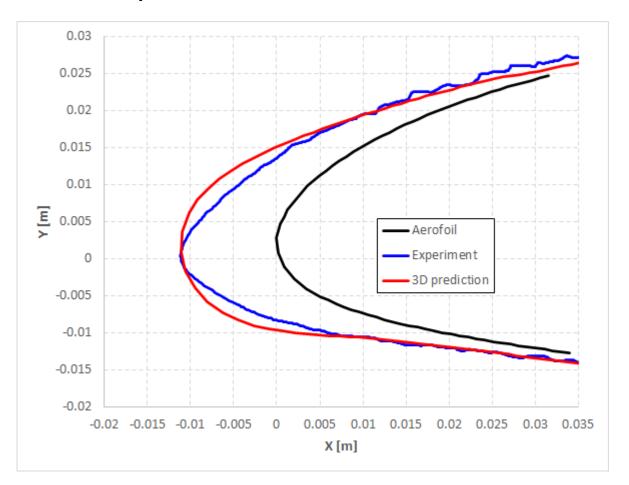


ICE ACCRETION CASES

Case 241 and 242

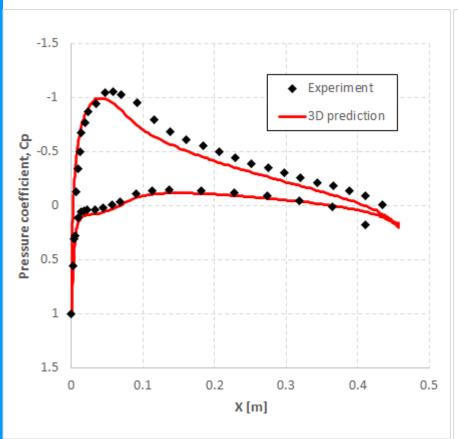
- 18-inch NACA23012, $\alpha = 2^{\circ}$
 - Case 241 is MVD = 30microns, LWC = 0.42g/m³, SAT = -23C
 - Case 242 is MVD = 15microns, LWC = $0.81g/m^3$, SAT = -7.1C
- Modelled within IRT, including walls (3D)
- 8.40 million cells

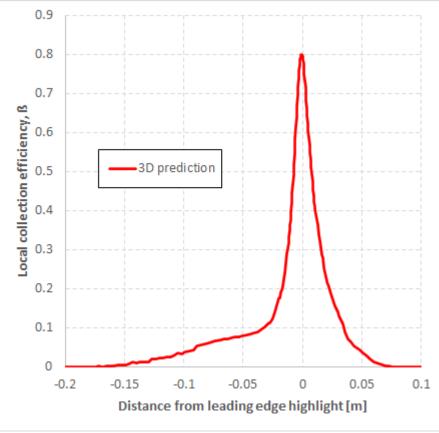
Ice shape



Ice mass = 0.36kg/m

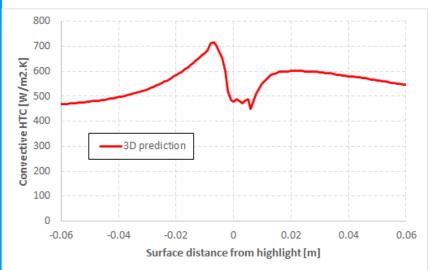
Case 241 (cont.)

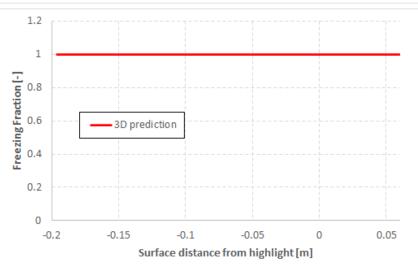


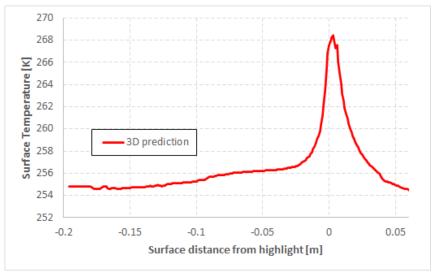


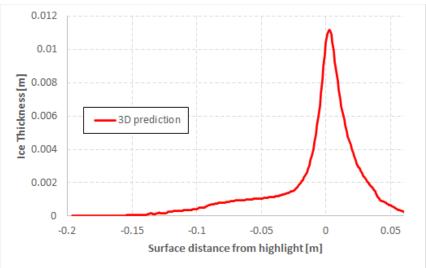


Case 241 (cont.)



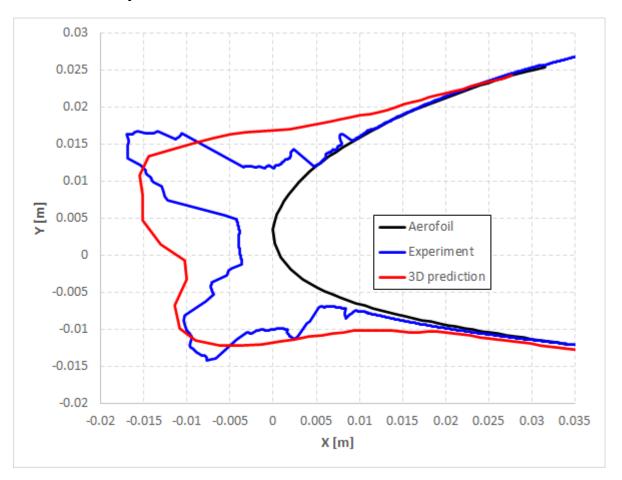








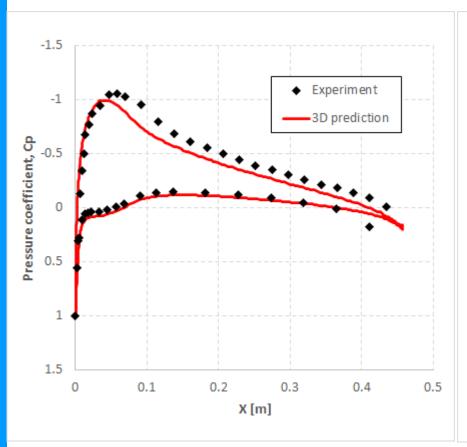
Ice shape

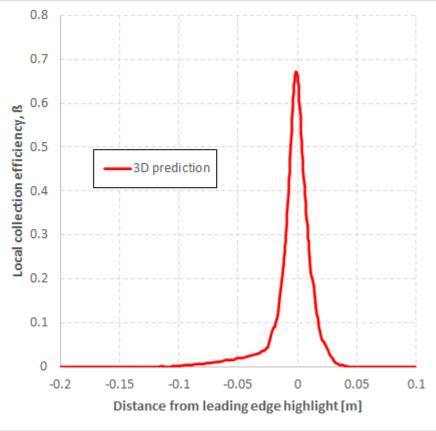


Ice mass = 0.35kg/m

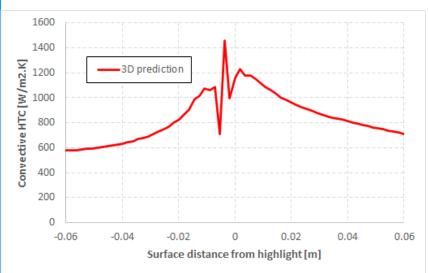


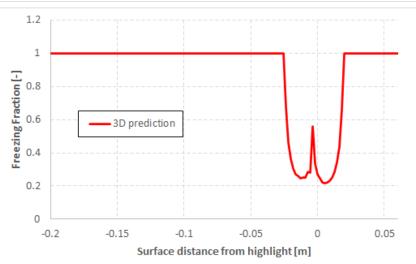
Case 242 (cont.)

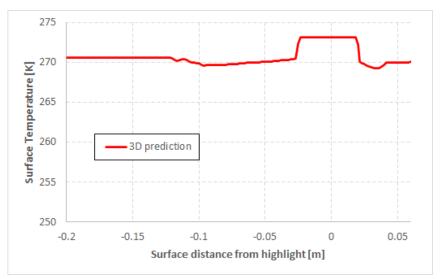


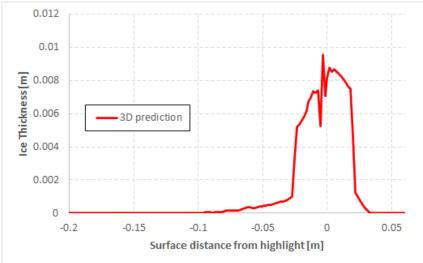


Case 242 (cont.)







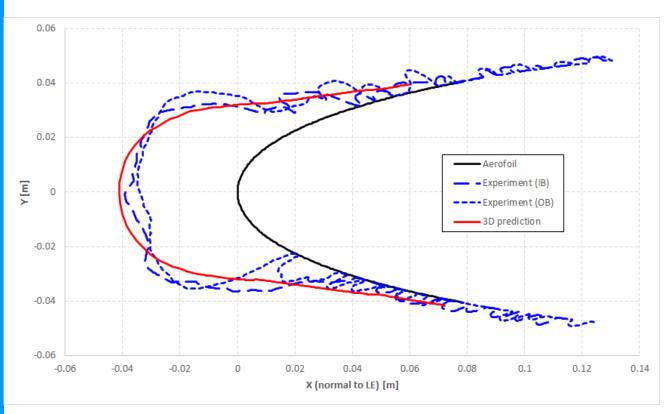




Case 361 and 362

- 30-degree swept NACA0012, $\alpha = 0^{\circ}$
 - Case 361 is SAT = -16.15C
 - Case 362 is SAT = -7.15C
- Both cases are MVD = 34.7microns, 0.5g/m³
- Modelled within IRT, including walls (3D)
- 11.80 million cells

Ice shape

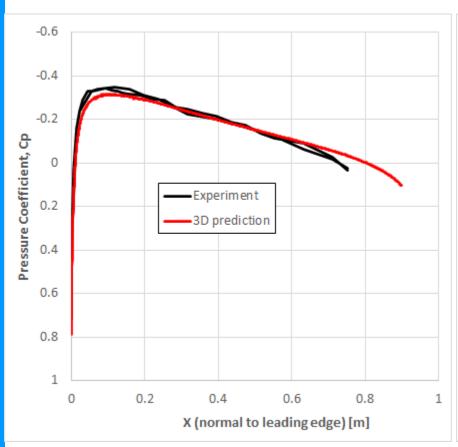


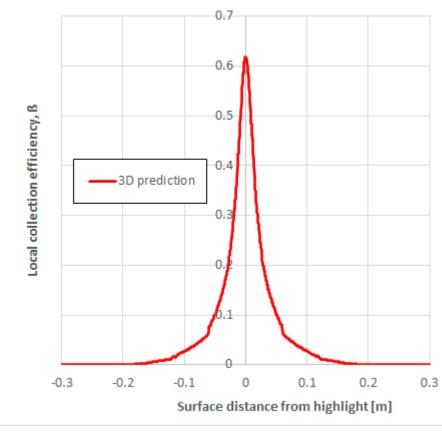
Ice mass = 2.23kg/m

Experiment = 1.9kg/m



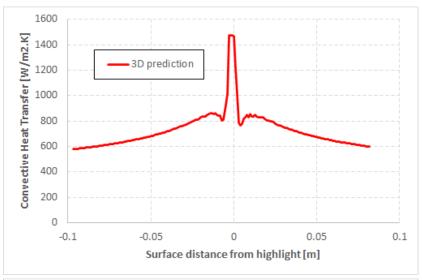
Case 361 (cont.)

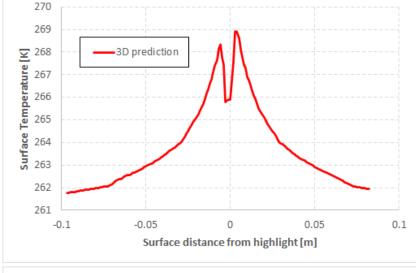


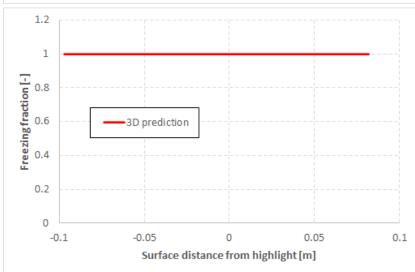


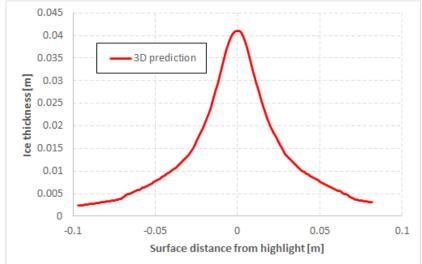


Case 361 (cont.)



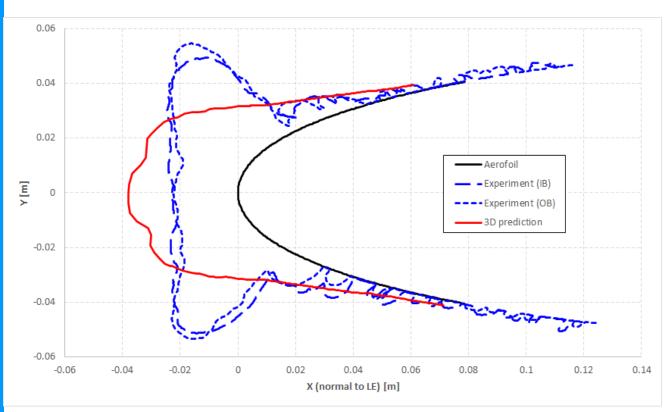








• Ice shape

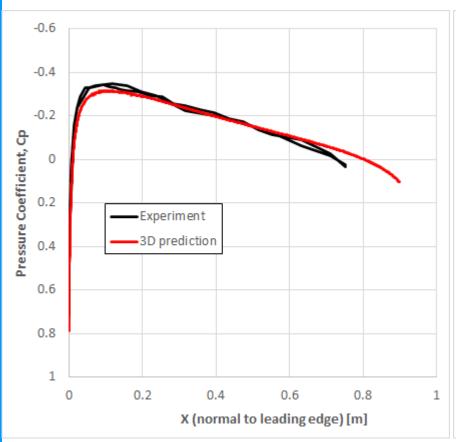


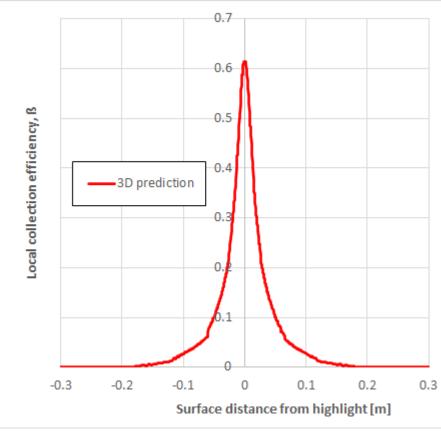
Ice mass = 2.13kg/m

Experiment = 1.62kg/m

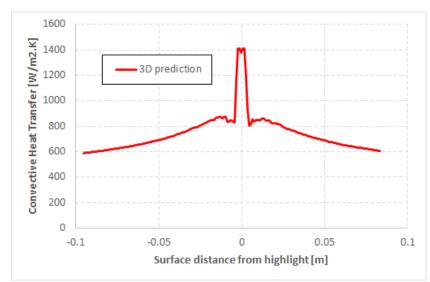


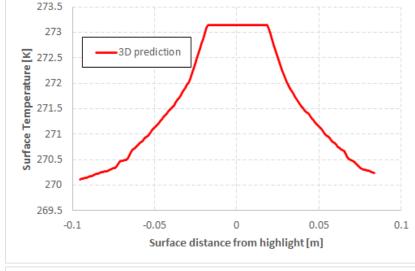
Case 362 (cont.)

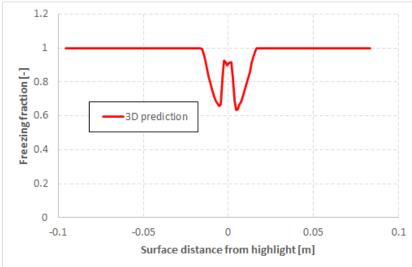


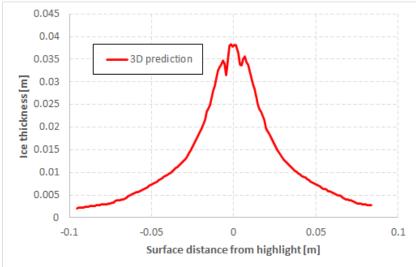


Case 362 (cont.)







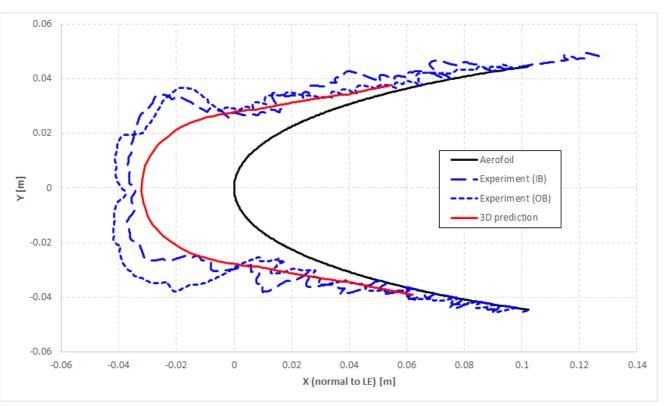




Case 371 and 372

- 45-degree swept NACA0012, $\alpha = 0^{\circ}$
 - Case 371 is SAT = -16.15C
 - Case 372 is SAT = -7.15C
- Both cases are MVD = 32microns, 0.5g/m³
- Modelled within IRT, including walls (3D)
- 11.78 million cells

Ice shape

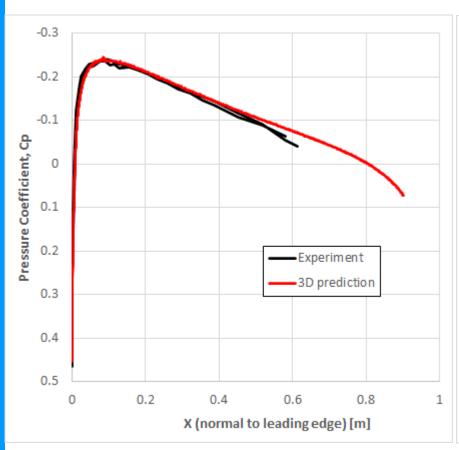


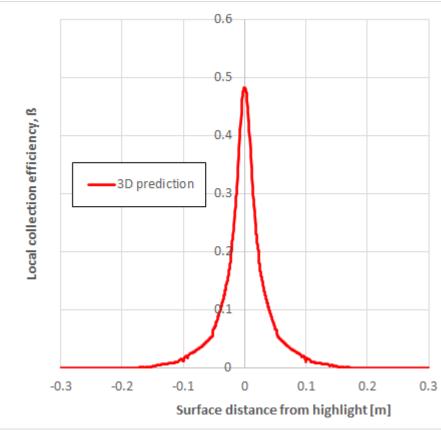
Ice mass = 2.04kg/m

Experiment = 1.58kg/m

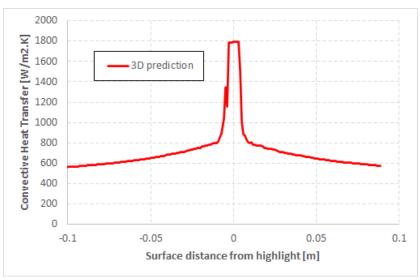


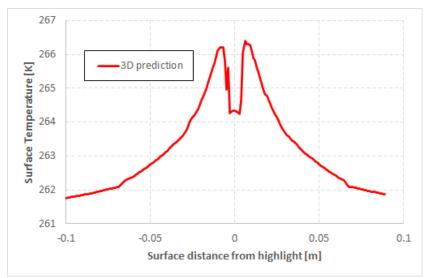
Case 371 (cont.)

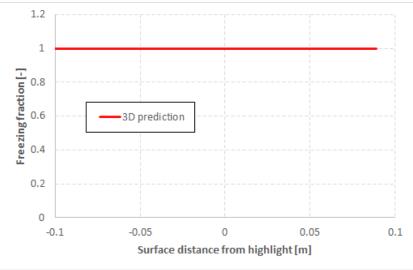


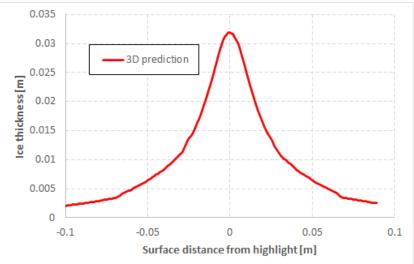


Case 371 (cont.)



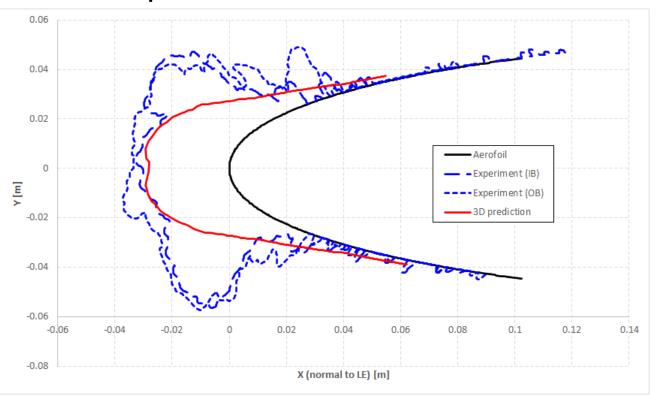








• Ice shape

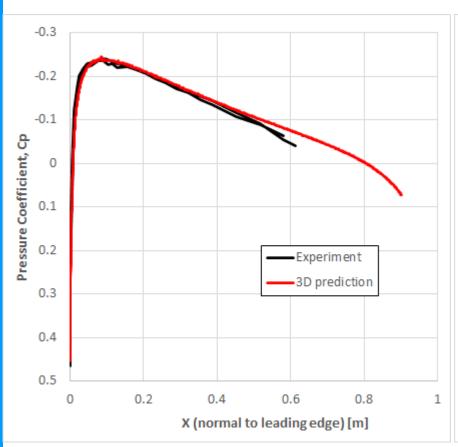


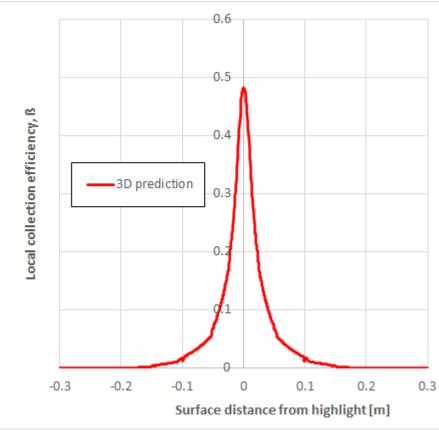
Ice mass = 1.93kg/m

Experiment = 1.60kg/m



Case 372 (cont.)







Case 372 (cont.)

